

## Reliability Analysis of Wind Turbine Blades Considering Lightning Strike

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> NAWEA/WindTech 2019 Conference October 15, 2019 University of Massachusetts Amherst, Amherst, Massachusetts



#### **Background & Motivation**





Lightning struck the blade tip. Information found online.

- Lightning strike damage accounts for  $\sim 23.4\%$  of wind turbine failure.
- Lightning strike protection cannot 100% prevent lightning damage;
- An accurate evaluation of wind turbines' reliability considering lightning strike is of critical importance.



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#### **Overview**

Root

Composite Materials «



- Tip Aft Shear Web Spar Cap **Forward Shear Web Trailing Edge** Leading Edge 50 m
- Parametric lightning stepped leader model
- Problem set up in COMSOL
- Reliability Analysis of Composite Wind Turbine Blades
- Design Optimization Considering Lightning Strike Damage



## Straight Lightning Stepped Leader Model

• Lightning-strike-induced electric field calculation by finite element models.





## **The Real Lightning Leader**



Artificial Lightning Arc Channel (High Voltage Lab at Mississippi State University)

Lightning in the Nature (Picture found online)

- Both the natural and artificial lightning channels show strong tortuosity.
- Fifty percent of the discharges exist two or three branches, and only twelve percent do not show any branch.



## Parametric Lightning Stepped Leader Model

- The azimuthal angle θ in the spherical coordinate follows uniformly distribution;
- The angle between two adjacent line segments φ follows a Gaussian distribution;
- The length of each segment follows a uniform distribution from 80m to 100m.





## Problem Setup in COMSOL

• The random generation procedure is terminated when the distance between the tip of the tortuous channel and the ground structure becomes smaller than the striking distance



Electric field due to **tortuous lightning leader model** calculation setup in COMSOL Multiphysics





- The generation of branches keep same;
- The upper bifurcation happens at the height near 2500m;
- The lower bifurcation occurs at the height approaching 1500m.



#### **Estimation of the Electric Field**

• Electric field magnitude distribution in the vicinity of wind turbine.





#### **FEA Result and Discussion**

• The magnitude of electric field on the vertical blade OA induced by three different lightning stepped leader models, LPL I.





#### **FEA Result and Discussion**

• The magnitude of electric field on the vertical blade OA induced by the tortuous lightning stepped leader models, LPL I, LPL II, LPL III.





#### **Reliability Analysis of Composite Wind Turbine Blades**





 The values of the peak current follow the log-normal distribution



#### **Estimation of Breakdown Strength and Safety Factor**

Dielectric breakdown strength of composite wind turbine blades

$$E_b = TI \cdot c_1 + c_2 / t,$$

- TI tracking index is highly dependent on the fiber orientation, fiber and matrix properties, surface defects and wide erosions.
- TI is not deterministic
- Dielectric breakdown is also dependent on the temperature
- $\Box E_b \text{ is considered only a function of laminate thickness } t.$





#### The Result of Reliability Analysis

• The average safety factor on the vertical blade OA induced by three different lightning stepped leader model considering the uncertainty of the peak current.





## Design Optimization<sup>1</sup>

- Optimization Design Considering Lightning Strike Damage
- Design variables laminate thicknesses



<sup>1</sup> W. Hu, W. Zhao, Y. Wang, Z. Liu\*, J. Cheng\*, and J. Tan, 2019, "Design Optimization of Composite Structures Considering 15 Tortuous Lightning Strike and Non-Proportional Multi-Axial Fatigue Damage", Engineering Optimization, accepted.



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## Design Optimization<sup>1</sup>

Optimization problem formulation

Minimize  $C(\mathbf{d}) = \left( c_{QQ1} \sum_{i}^{12} m_i^o \frac{d_i}{d_i^o} \right) / C^o$ Subject to  $G_i(\mathbf{d}) = 1 - L_i(\mathbf{d}) = 1 - \frac{E_{bi}(\mathbf{d})}{E_i} \le 0, \ i = 1, 2, ..., NL$  Lightr

Lightning Constraints

$$G_{j}(\mathbf{d}) = D_{20year}^{j}(\mathbf{d}) - 1$$
Fatigue Constraints
$$= 52560 \times 20 \times \sum_{i}^{12} \sum_{j}^{50} \overline{P}_{VI}^{i,j}(v_{10}^{i}, i_{10}^{i}) D_{10}^{i,j}(\mathbf{d}, v_{10}^{i}, i_{10}^{i}) - 1 \le 0, \ j = 1, 2, ..., NF$$

$$\mathbf{d}^{L} \leq \mathbf{d} \leq \mathbf{d}^{U}, \quad \mathbf{d} \in \mathbb{C}^{NDV}$$



<sup>1</sup> W. Hu, W. Zhao, Y. Wang, Z. Liu\*, J. Cheng\*, and J. Tan, 2019, "Design Optimization of Composite Structures Considering 16 Tortuous Lightning Strike and Non-Proportional Multi-Axial Fatigue Damage", Engineering Optimization, accepted.



# THANK YOU Q & A